

RCC Structure – Footing

Case Example:

Analyze a 3000mm x 3000mm square footing with 650 mm over all depth for a 450mm x 450 mm column subjected to 1200 kN dead load and 500 kN imposed load. Consider soil bearing pressure 200 kN/m², Concrete grade M20 and Fe415 steel 25 mm diameter 10 bars in each direction with 50 mm clear cover.

Analysis:

Data:

Characteristic strength of concrete $f_{ck} = 20 \text{ N/mm}^2 = 20 \times 10^3 \text{ kN/m}^2$

Yield strength of steel = 415 N/mm² = 415 × 10³ kN/m²

Steel area $A_s = 0.25\pi \times 25^2 \times 10 = 4909 \text{ mm}^2$

Footing dimension = 3000mm x 3000mm x 650mm

Footing area: 3m x 3m = 9 m²

Percent steel $p_t = A_s \times 100 / (650 \times 3000) = 0.252\%$

A. Footing Factored Load:

- (i) DL = 1200 kN
- (ii) Imposed load = 500 kN
- (iii) Factored load $P = (DL + LL) \times \text{load factor} = 2550 \text{ kN}$

B. Effective depth (d):

Footing thickness – clear cover – bar dia₁ – bar dia₂/2 = 650 – 50 – 25 – 25/2 = 562.5 mm

C. One-way shear

- (i) Design shear of concrete $\tau_c = 0.36 \text{ N/mm}^2$ (Refer table 19 IS 456 for τ_c for given percent steel 0.252%)
- (ii) Critical section for one-way shear is at distance 'd' from the face of the column
- (iii) Shear force V acting at this section is given by = $(P/2L) \times (L - a - 2d) = (2550 \times 10^3 / 2 \times 3000) \times (3000 - 450 - 2 \times 562.5) = 615 \times 10^3$
- (iv) For equilibrium $V = \tau \times L \times d$
- (v) $\tau = 615 \times 10^3 / (3000 \times 562.5) = 0.36 \text{ kN/mm}^2$ that is same as τ_c

D. Two-way (punching) shear

- (i) Critical section for two-way shear is at a distance $d/2$ from the face of the column all around as shown in figure 13 A and 13B IS : 456. Accordingly shear area $A_p = 4(a+d)d = 4(0.450 + 0.5625) \times 0.5625 = 2.278 \text{ m}^2$
- (ii) Shear force $V = A_p \times \tau_p \text{ kN}$
- (iii) For equilibrium $V = (P/L^2)(L^2 - (a+d)^2) = (2550/3^2) \times (3^2 - (0.45 + 0.562)^2) = 2259.8 \text{ kN}$
- (iv) We get $\tau_p = V / A_p = 2259.8 / 2.278 = 0.99 \times 10^3 \text{ kN/m}^2 = 0.99 \text{ N/mm}^2$
- (v) Design punching shear given as $0.25\sqrt{f_{ck}} = 1.12 \text{ N/mm}^2$ that is $> \tau_p$ calculated

E. Moment and Capacity:

- (i) Moment at the face of the column $M_u = (P/L^2)(L(L-a)^2/8) = (2550/3^2)(3(3-0.45)^2/8) = 690.89 \text{ kNm}$
- (ii) Moment capacity $M_{\max} = 0.138 f_{ck}.b.d^2 = 0.138*20e3*3*0.562^2 = 2615 \text{ kNm}$
- (iii) Moment capacity is greater than moment applied at the face of the column.

F. Check Development Length (Clause 26.2.1 IS 456)

- (i) $L_d = (\phi*\sigma_s)/(4*\tau_{bd})$
- (ii) Design Bond strength τ_{bd} for M20 is given as $1.2 \times 1.6 \text{ N/mm}^2$ (added 60% for Tor-rods)
- (iii) $\therefore L_d = (25*415)/(4*1.92) = 1351 \text{ mm}$

G. Footing Analysis Summary

- (i) Footing pressure: $1700 \text{ kN}/9 \text{ m}^2 = 188.9 \text{ kN/m}^2 < \text{soil bearing pressure.}$
- (ii) Footing depth is sufficient to resist both One-way and Two-way shear as per critical section mentioned in the code.
- (iii) Thickness is sufficient to resist bending moment without compression steel in the footing.
- (iv) Percent steel (0.252%) exceeds minimum prescribed as per Clause 26.5.2.1

H. Material Estimates

- (i) Concrete volume: $3^2*0.650 = 5.85 \text{ m}^3$
 - (ii) Cement quantity: M20 Volume of cement 1:5.5 = $5.85*1440/5.5 = 1532 \text{ kg}$
 - (iii) Steel quantity: ϕ -25 mm x 60m length $\approx 233 \text{ kg}$
- Add necessary allowances for wastage, shrinkage etc. to the above estimates.